

Selecting the appropriate band cylinder is simple. The information you need includes:

- the stroke,
- the force required for moving the load,
- the weight of the load,
- the position of the load (centered on the carrier or elsewhere),
- the final or average velocity.

How to select

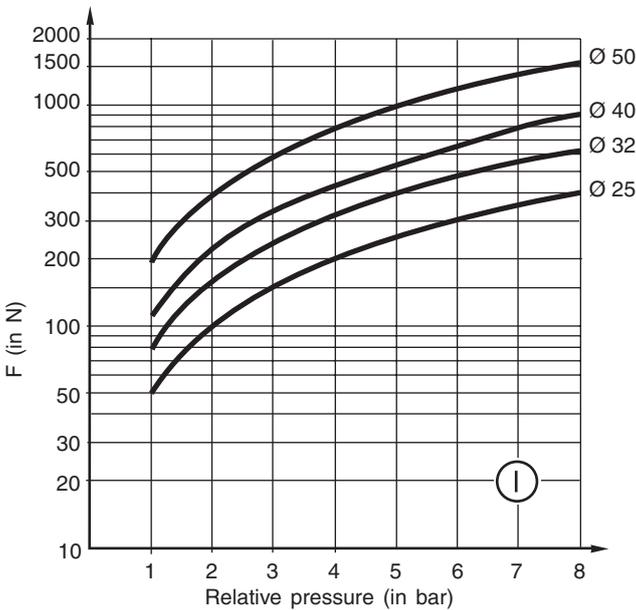
Graph ① represents the theoretical force at various pressures. For the most efficient use of a cylinder, it is recommended to use a load rate of 70 %: the force needed to move the load therefore corresponds to 70% of the theoretical force.

After defining the cylinder diameter, you must determine if the cylinder's internal cushions can be used.

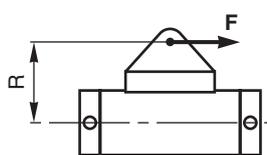
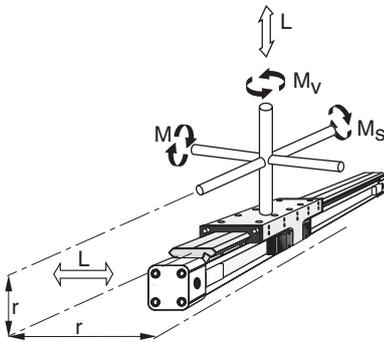
Allowable bending moments

A bending moment will occur if the load is not centered on the carrier (see bending moment data below).

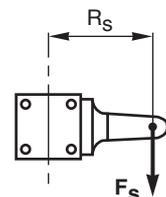
THEORETICAL FORCE AT VARIOUS PRESSURES



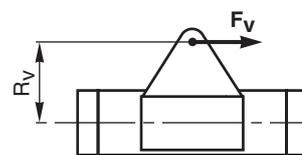
ALLOWABLE BENDING/TWISTING MOMENTS



$$M = F \times R$$



$$M_s = F_s \times R_s$$



$$M_v = F_v \times R_v$$

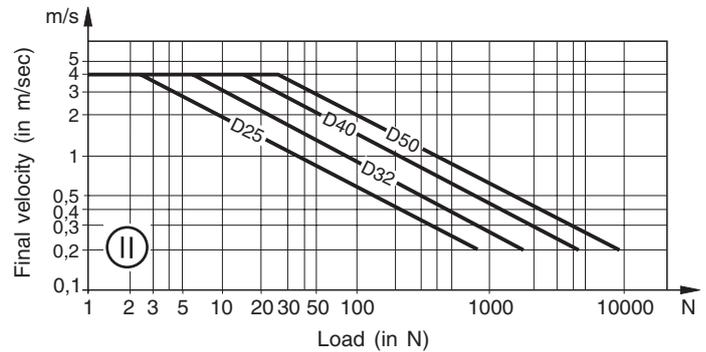
Cushioning capacity

Graph ② is used to determine the type of cushioning needed. If the intersection point of the final velocity and the load falls below the curves, the internal cushions are adequate. If this is not the case, you must either choose a larger cylinder with greater cushion capacity, or use the shock absorbers which are available as an accessory. If you have determined that the internal cushions would be used near their maximum capacity and there is highly intense movement, it would be wise to use the optional shock absorbers.

OTHER ACCESSORIES:

- Tube support brackets: **You must determine if intermediate tube support brackets are required**, depending on the weight of the charge and the stroke. (see chart on tube support sheet).
- Reed switch or magneto-inductive detectors for position control.

CUSHION DATA



The velocities indicated in graph ② represent **final velocities**. To properly determine the inertial forces for cushioning, it is important to know the **final velocity**.

If final (or impact) velocity cannot be calculated directly, a reasonable guideline is:

$$\text{Final V} = 1,5 \times \text{average velocity}$$

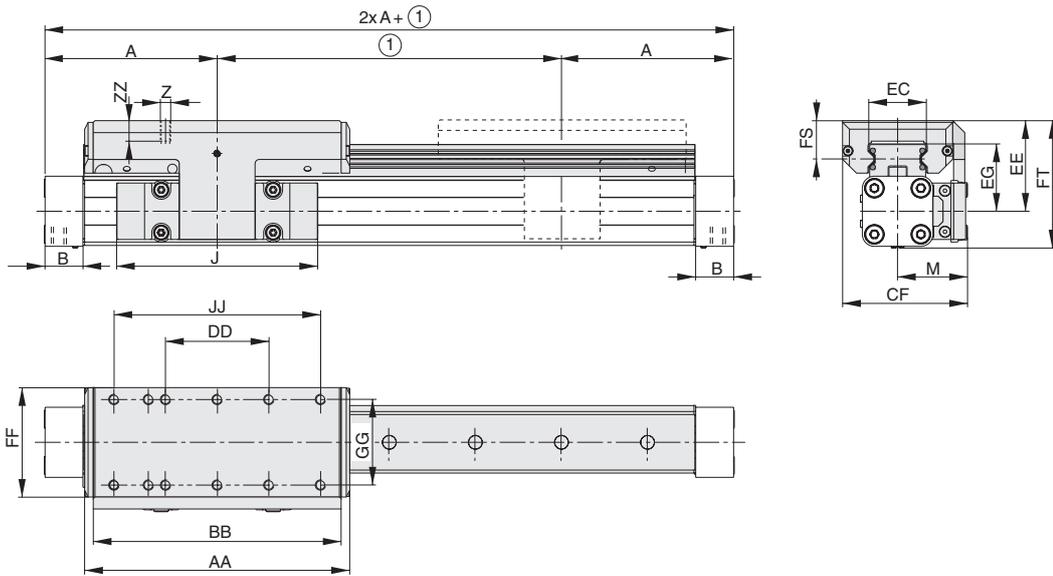
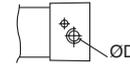
Ø Cylinder (mm)	Bending moments (in N.m)			Load (in N) L	Carrier weight (in kg)
	M	M _s	M _v		
25	39	16	39	857	0,75
32	73	29	73	1171	1,18
40	158	57	158	2074	1,70
50	249	111	249	3111	2,50

Note: When using the cushioning diagram, be sure to add the weight of the carrier (and that of the brake) to the weight of the load to be moved.

DIMENSIONS AND WEIGHTS

BARE CYLINDERS

Bottom view



① : stroke

Bore (mm)	DIMENSIONS (mm)																			Cylinder weight (kg)		Carrier weight (kg)
	A	B	D	J	M	Z	AA	BB	DD	CF	EC	EE	EG	FF	FS	FT	GG	JJ	ZZ	(1)	(2)	(3)
25	100,4	22	G1/8	117	40,5	M6	154	144	60	72,5	32,5	53	39	64	23	73,5	50	120	12	1,65	0,40	0,75
32	125,2	25,5	G1/4	152	49	M6	197	187	80	91	42	62	48	84	25	88	64	160	12	3,24	0,62	1,18
40	150	28	G1/4	152	55	M6	232	222	100	102	47	64	50,5	94	23,5	98,5	78	200	12	4,35	0,70	1,70
50	175	33	G1/4	200	62	M6	276	266	120	117	63	75	57	110	29	118,5	90	240	16	7,03	0,95	2,50

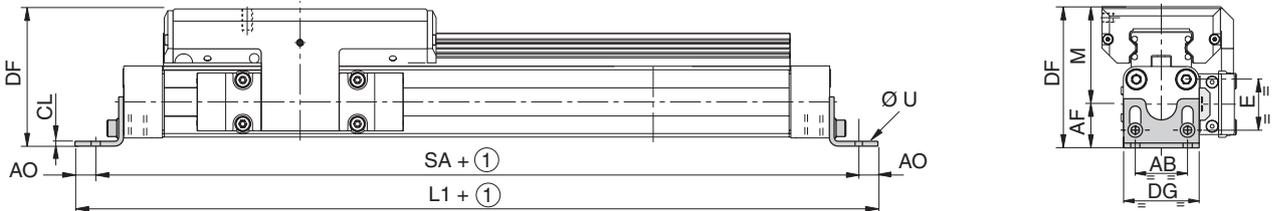
(1) Weight with 0 mm stroke

(2) Weight to be added per additional 100 mm length

(3) When using the cushioning diagram, be sure to add the weight of the carrier to the weight of the load to be moved.

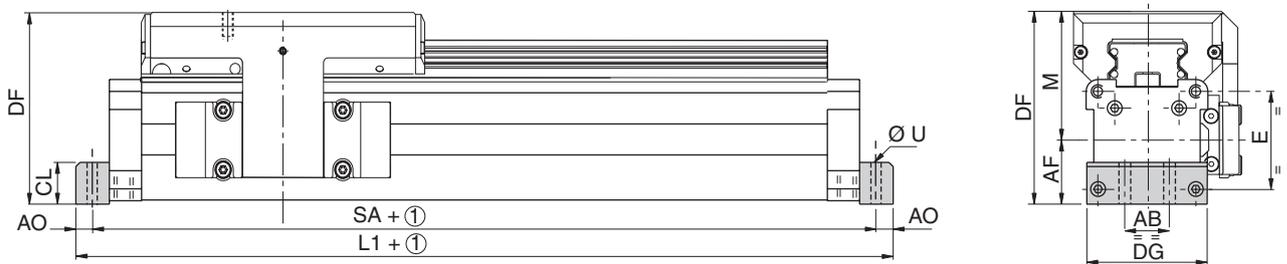
CYLINDER WITH MOUNTING BRACKETS

Ø25 - 32 mm



CYLINDER WITH MOUNTING FLANGES

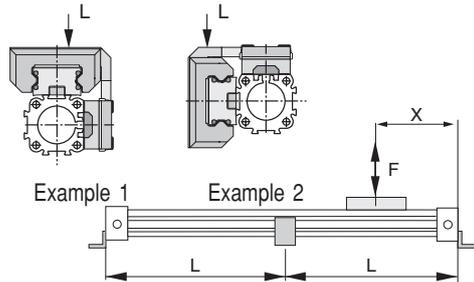
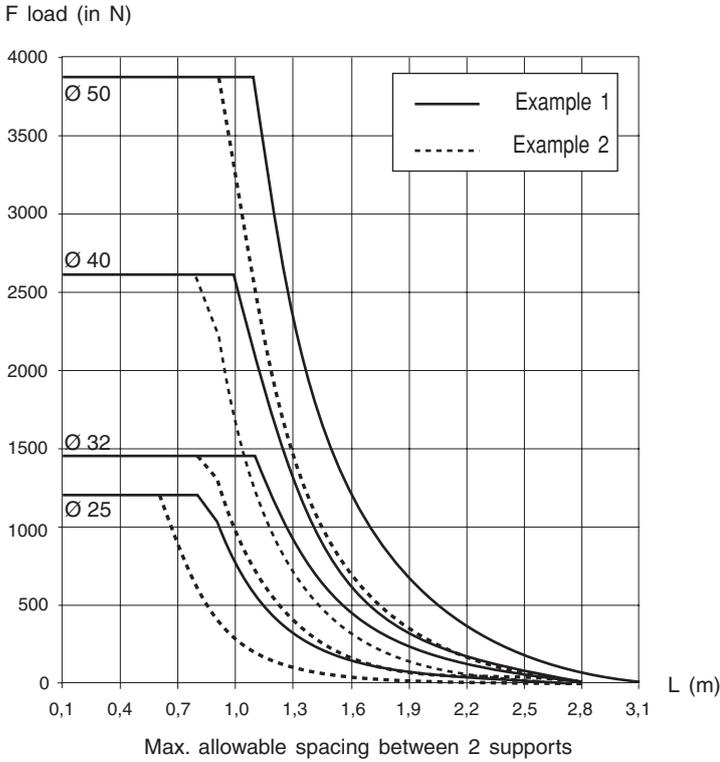
Ø40 - 50 mm



① : stroke

Bore (mm)	DIMENSIONS (mm)														Weights (kg)	
	AB	AF min	AF max	A0	CL	DF min	DF max	DG	E	L1	M	SA	U	Brackets	Flanges	
25	27	22,7	32,3	9,5	2,5	75,7	85,3	39	27	250,8	53	231,8	6,6	0,072	-	
32	36	32,5	45,2	9,3	3	94,5	107,2	50	36	292,4	62	273,8	7	0,117	-	
40	30	35,2		11,3	24	99,2		68	54	348	64	325,4	9	-	0,210	
50	31,8	46		16,2	30	121		86	70	398	75	365,6	10	-	0,308	

For certain strokes and loads, it is necessary to use tube support brackets for intermediate support. The graph below is used to determine the maximum allowable support spacings depending on the load and the number of supports required. These supports are made of treated light alloy and are designed to fit into the dovetail grooves which run the length of the cylinder tube.



Number of supports needed (n) given that the cylinder is fixed on the ends.

$$n = \left(\frac{\text{Stroke} + 2 X}{L} \right) - 1$$

n = whole number, rounded up.

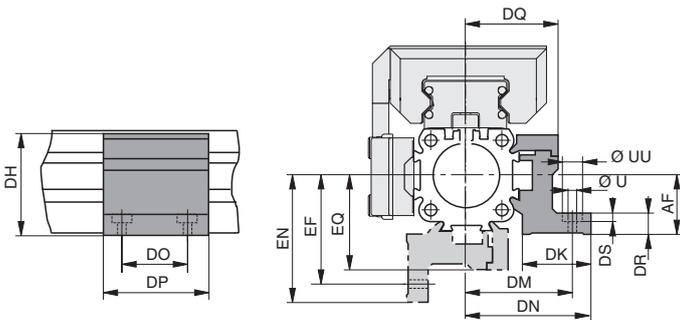
X = A dimension in mm, mentioned with general cylinder dimensions

L = max. distance defined in the adjacent graph.

CHOICE OF EQUIPMENT

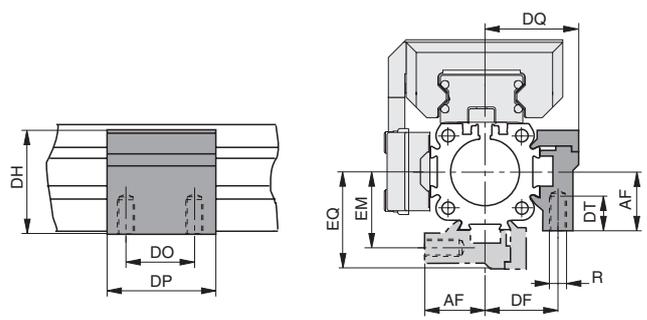
The tube supports must be mounted into the dovetail rails on the cylinder as shown below.

Top mounting



Bore (mm)	CODE	Weights (kg)
25	43400501	0,130
32	43400502	0,160
40	43400503	0,161
50	43400504	0,189

Bottom mounting



Bore (mm)	CODE	Weights (kg)
25	43400508	0,061
32	43400509	0,073
40	43400510	0,140
50	43400511	0,169

DIMENSIONS

Bore (mm)	DIMENSIONS (mm)																		
	R	U	UU	AF	DF	DH	DK	DM	DN	DO	DP	DQ	DR	DS	DT	EF	EM	EN	EQ
25	M5	5,5	10	25	27	41	26	40	47,5	36	50	34,5	11	5,7	10	41,5	28,5	49	36
32	M5	5,5	10	33	33	49	27	46	54,5	36	50	40,5	13	5,7	10	48,5	35,5	57	43
40	M6	7	-	35,2	35	58,2	34	53	60	45	60	45	7,2	-	11	56	38	63	48
50	M6	7	-	46	40	69	34	59	67	45	60	52	8	-	11	64	45	72	57